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| 20 | SUPPLEMENTAL MATERIAL  |
| 21 | Pages -12; Tables – 2; Figures - 4   |
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Runoff under natural rainfall from small tall fescue catchments in the

# **Materials and Methods**

| 2  | Standard Precipitation Index and drought classification. We used the Standard                 |
|----|---|
| 3  | Precipitation Index (SPI) approach (McKee et al. 1993; Edwards and McKee 1997;                |
| 4  | Hayes and Svoboda 1999; NDMC 2012a) to compare actual rainfall during the study               |
| 5  | aggregated at 1-, 3-, 6-, 9-, and 12-month time scales to the probability of rainfall for the |
| 6  | same time period based on 75 years of monthly rainfall records (1937-2011). A 1-month         |
| 7  | time scale analysis utilizes the total precipitation for that month, while a 3-month          |
| 8  | considers the month of interest and the two previous months, etc. The SPI approach has        |
| 9  | received widespread acceptance in recent years due to, among other traits, its simplicity     |
| 10 | (requiring only precipitation data), flexibility (computation at different time scales and    |
| 11 | hence use in a range of meteorological, hydrological and agricultural applications) and its   |
| 12 | probabilistic nature (Jain et al. 2010; Hayes 2000 and 2012). It is being used by the         |
| 13 | National Drought Mitigation and National Climatic Data Centers to table one- and              |
| 14 | multiple-month drought classifications across the United States. The developers               |
| 15 | recommend a minimum of 30 years of good quality monthly rainfall data to derive the           |
| 16 | SPI. The monthly rainfall values are first fitted into a suitable distribution such as the    |
| 17 | Gamma distribution. The estimated parameters are then used for calculating cumulative         |
| 18 | probability distribution for the time scale of interest and subsequently modified to include  |
| 19 | the common no rainfall occurrences. The ensuing cumulative probability is then                |
| 20 | transformed to the standard normal variable with mean of zero and variance of one. The        |
| 21 | SPI is the number of standard deviations (negative representing dry and positive wet          |
| 22 | conditions) the rainfall of interest is from the zero mean. For practical purposes SPI        |
| 23 | values encompassing the extremely dry to extremely wet spectrum have been classified          |

into categories (McKee et al. 1993; NDMC 2012b) representing intensities of dryness and wetness as: extremely dry (< -2.0), severely dry (-1.99 to -1.5), moderately dry (-1.49 to -1.0), near normal (-0.99 to 0.99), moderately wet (1.0 to 1.49), very wet (1.5 to 1.99), and extremely wet (> 2.0). Data Analyses. Data analyses for runoff in mm and normalized as percent of event rainfall (referred to as percent runoff) were carried out in three phases. In the first phase, we developed a methodology to estimate missing runoff values. First, using all available runoff data, linear regression was performed between all paddock-pairs. Following that, we identified for each paddock up to three other paddocks that gave the greatest group of coefficient of determination (r<sup>2</sup>). We then plotted the data from the three chosen paddock-pairs and checked if non-linear regression would improve any of the correlations. If so, we replaced a linear model with a non-linear one. Of the finally selected models, 75% were linear while 25% were non-linear, and 96% had  $r^2 \ge 0.8$  while 62% had  $r^{2} \ge 0.9$ . Two models had  $r^2$  of 0.71 and 0.74. A missing runoff value for a paddock was then estimated using the model from the paddock-pair that produced the greatest correlation if there was data from the corresponding paddock for the particular event; if not, the model and data from paddock-pair giving the next greatest correlation was used, etc. Usually no more than 2 steps were needed to estimate missing runoff data. In the second phase of data analyses, we examined possible correlations between runoff and landscape attributes generated from the detailed GPS/GIS-based survey because of the degree of runoff variability observed among individual paddocks. The ratio between the largest and smallest overall paddock mean runoff using the dataset with missing values, and that with estimate for missing values, varied from 3.6 to 4.2. First a

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stepwise regression was performed using rain, area-weighted slope, and lengths of each of the six categories of flow-path orders or some of them. Next a linear regression was performed between runoff and length of each of the six flow path order categories, cumulative percentage area by slope class of 1 to 9 in increments of 1%, and areaweighted slope. Following that, a regression of runoff against a combination of areaweighted slope and length of one of the six flow path order categories, and a combination of flow path order 1 (FPO1) and cumulative percentage area up to slope class 2 (CPS2) was performed. The latter was done because, individually, these two variables showed greater correlation with runoff than the other considered variables. Finally in this phase, we performed factor analysis using 23 variables describing rainfall, runoff, and landscape attributes and identified event rainfall amount, FPO1, CPS2, and area-weighted slope (AWS) as the best variables to account for the effects of landscape on runoff variability. Two of these, FPO1 and CPS2, were variables that showed greater correlation with runoff in the analyses performed earlier. We, therefore, used these four variables as covariates in the third phase, the statistical analysis, to constrain the analysis into identifying treatment effects only as described in the main article.

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**Supplemental Table 1**Runoff flow path lengths and slope attributes by paddock from detailed GPS/GIS-based survey.

| Landscape Paddock† |         |       |       |       |       |       |       |       |       |       |       |       |       |       |
|--------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Attribute‡         | BF12    | BW10  | IM11  | BF5   | IMHA  | BM9   | BW4   | IW2   | IW8   | IM6   | IF3   | IMHB  | IF7   | BM1   |
| meter              |         |       |       |       |       |       |       |       |       |       |       |       |       |       |
| FPO1               | 904     | 750   | 1148  | 1587  | 1189  | 1099  | 1943  | 1953  | 1334  | 1425  | 1133  | 2136  | 1134  | 2540  |
| FPO2               | 570     | 362   | 457   | 501   | 598   | 596   | 864   | 754   | 619   | 568   | 370   | 840   | 500   | 839   |
| FPO3               | 254     | 200   | 180   | 181   | 156   | 183   | 276   | 208   | 241   | 241   | 119   | 188   | 120   | 267   |
| FPO4               | 106     | 26    | 93    | 107   | 39    | 48    | 111   | 24    | 33    | 135   | 34    | 85    | 24    | 46    |
| FPO5               | 0       | 0     | 0     | 33    | 0     | 0     | 0     | 0     | 42    | 30    | 0     | 79    | 0     | 0     |
| TFPL               | 1833    | 1337  | 1844  | 2409  | 1977  | 1926  | 3194  | 2939  | 2269  | 2400  | 1656  | 3325  | 1779  | 3692  |
|                    | percent |       |       |       |       |       |       |       |       |       |       |       |       |       |
| CPS1               | 1.5     | 7.5   | 3.1   | 0.4   | 7.0   | 0.9   | 9.6   | 2.2   | 5.0   | 0.6   | 2.1   | 1.2   | 3.8   | 3.9   |
| CPS2               | 19.1    | 36.7  | 33.9  | 13.2  | 18.9  | 12.5  | 23.0  | 10.0  | 16.0  | 11.6  | 15.6  | 6.5   | 9.9   | 13.4  |
| CPS3               | 36.3    | 65.8  | 52.3  | 39.9  | 29.6  | 36.7  | 40.0  | 24.0  | 34.4  | 51.1  | 43.7  | 26.6  | 24.2  | 26.9  |
| CPS4               | 61.6    | 78.2  | 67.7  | 68.6  | 48.2  | 52.6  | 56.5  | 40.7  | 52.7  | 94.3  | 61.1  | 62.1  | 62.8  | 43.8  |
| CPS5               | 83.5    | 87.7  | 82.9  | 94.2  | 64.4  | 62.3  | 69.8  | 64.3  | 71.4  | 100.0 | 73.7  | 76.9  | 88.7  | 58.0  |
| CPS6               | 90.6    | 95.6  | 95.3  | 100.0 | 79.6  | 83.9  | 85.3  | 84.1  | 95.3  | *     | 84.5  | 100.0 | 95.0  | 79.3  |
| CPS7               | 95.0    | 99.5  | 100.0 | *     | 95.1  | 100.0 | 93.4  | 95.0  | 96.9  | *     | 94.4  | *     | 97.8  | 94.2  |
| CPS8               | 99.6    | 100.0 | *     | *     | 98.1  | *     | 98.6  | 100.0 | 100.0 | *     | 100.0 | *     | 99.6  | 98.6  |
| CPS9               | 100.0   | *     | *     | *     | 100.0 | *     | 100.0 | *     | *     | *     | *     | *     | 100.0 | 100.0 |
| percent            |         |       |       |       |       |       |       |       |       |       |       |       |       |       |
| AWS                | 4.1     | 3.3   | 3.6   | 3.8   | 4.6   | 4.5   | 4.2   | 4.8   | 4.3   | 3.4   | 4.3   | 4.3   | 4.2   | 4.8   |

<sup>†</sup> Columns are arranged by ascending order (left to right) of paddock geometric mean runoff. Paddock designation: 1<sup>st</sup> letter – fertilizer treatment (B – broiler litter, and I – inorganic fertilizer); 2<sup>nd</sup> letter – fescue treatment (F – Free, W –Wild, and M – MaxQ). 3<sup>rd</sup> letter or numerals (H – hayed, 1 to 12 grazed paddock numbers); 4<sup>th</sup> letter – hayed paddocks A & B. Cells with asterisks indicate absence of the corresponding attribute.

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<sup>‡</sup> FPO1-FPO5. Runoff flow path order 1 to 5

TFPL. Total flow path length

CPS1 to CPS9. Cumulative percentage area of paddock for slope class 1 to 9

AWS. Area-weighted slope in percent

Supplemental Table 2

Summary of two-sample t-test for LN-transformed runoff and percent runoff dataset with missing values (Missing) and dataset with missing values filled in through regression

4 (Filled) †

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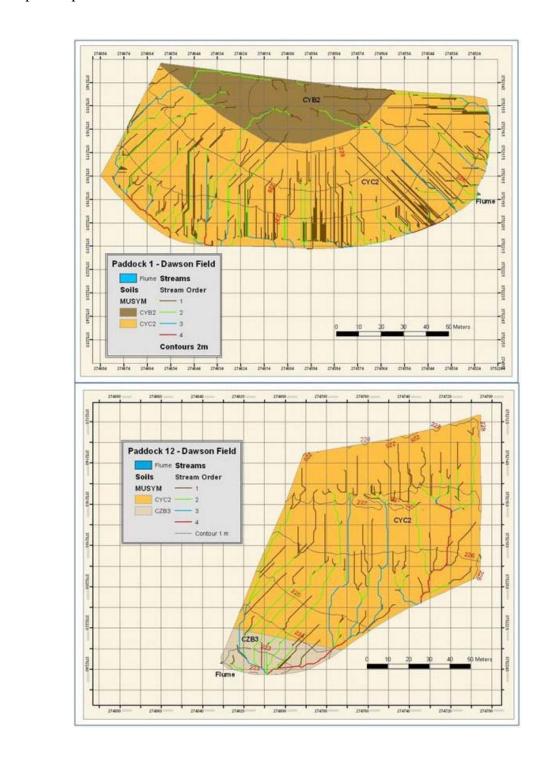
| (Pilled) †     |       | Missing |    |       |       |    |        |
|----------------|-------|---------|----|-------|-------|----|--------|
| Paddock        | Mean  | SE      | n  | Mean  | SE    | n  | Pr > F |
| Runoff         |       |         |    |       |       |    |        |
| BM1            | 1.874 | 0.129   | 67 | 1.848 | 0.121 | 77 | 0.886  |
| IW2            | 1.260 | 0.248   | 34 | 1.276 | 0.154 | 77 | 0.956  |
| IF3            | 1.618 | 0.153   | 69 | 1.676 | 0.144 | 77 | 0.783  |
| BW4            | 1.259 | 0.150   | 65 | 1.335 | 0.138 | 77 | 0.711  |
| BF5            | 1.090 | 0.264   | 25 | 1.124 | 0.137 | 77 | 0.907  |
| IM6            | 1.448 | 0.152   | 73 | 1.392 | 0.147 | 77 | 0.793  |
| IF7            | 1.696 | 0.301   | 17 | 1.537 | 0.128 | 77 | 0.632  |
| IW8            | 1.358 | 0.186   | 58 | 1.366 | 0.152 | 77 | 0.972  |
| BM9            | 1.187 | 0.138   | 70 | 1.162 | 0.132 | 77 | 0.896  |
| BW10           | 0.853 | 0.131   | 62 | 0.774 | 0.115 | 77 | 0.650  |
| IM11           | 0.878 | 0.131   | 59 | 0.879 | 0.114 | 77 | 0.994  |
| BF12           | 0.814 | 0.143   | 61 | 0.824 | 0.126 | 77 | 0.957  |
| IMHA           | 1.105 | 0.127   | 58 | 1.228 | 0.111 | 77 | 0.470  |
| IMHB           | 1.676 | 0.303   | 25 | 1.876 | 0.135 | 77 | 0.551  |
| Percent runoff |       |         |    |       |       |    |        |
| BM1            | 2.537 | 0.127   | 67 | 2.528 | 0.115 | 77 | 0.955  |
| IW2            | 1.586 | 0.282   | 34 | 1.678 | 0.167 | 77 | 0.772  |
| IF3            | 2.162 | 0.166   | 69 | 2.235 | 0.154 | 77 | 0.749  |
| BW4            | 1.670 | 0.172   | 65 | 1.764 | 0.157 | 77 | 0.686  |
| BF5            | 1.338 | 0.296   | 25 | 1.460 | 0.159 | 77 | 0.708  |
| IM6            | 1.881 | 0.169   | 73 | 1.803 | 0.166 | 77 | 0.743  |
| IF7            | 2.135 | 0.311   | 17 | 2.061 | 0.140 | 77 | 0.824  |
| IW8            | 1.732 | 0.205   | 58 | 1.770 | 0.170 | 77 | 0.887  |
| BM9            | 1.560 | 0.161   | 70 | 1.530 | 0.152 | 77 | 0.895  |
| BW10           | 1.155 | 0.146   | 62 | 1.039 | 0.129 | 77 | 0.554  |
| IM11           | 1.193 | 0.148   | 59 | 1.203 | 0.127 | 77 | 0.960  |
| BF12           | 1.044 | 0.163   | 61 | 1.044 | 0.143 | 77 | 1.000  |
| IMHA           | 1.554 | 0.141   | 58 | 1.733 | 0.120 | 77 | 0.333  |
| IMHB           | 2.102 | 0.331   | 25 | 2.479 | 0.145 | 77 | 0.304  |

<sup>†</sup> SE – standard error. Percent runoff is runoff normalized with respect to event rainfall (runoff as percent of event rainfall). The row data were transformed as LN(runoff+1) and LN(percent runoff+1) for statistical analysis. In the Filled section, n of 77 includes events with zero runoff for the 77 storms that produced runoff in one or more paddocks at the same time.

GPS/GIS analysis-based soil, elevation contour, and stream order (runoff flow path order) map for paddock 1 (BM1 – broiler litter fertilization and MaxQ tall fescue) and paddock 12 (BF12 – broiler litter and Free tall fescue). Paddock 1 has ~2.8 times the stream order 1 (FPO1 - runoff flow path order 1) and ~1.5 the stream order 2 length as that of Paddock 12. A line of old terrace remnants can be discerned in the upper and middle part of paddock 12 from where stream order 1 feeds into stream order 2.

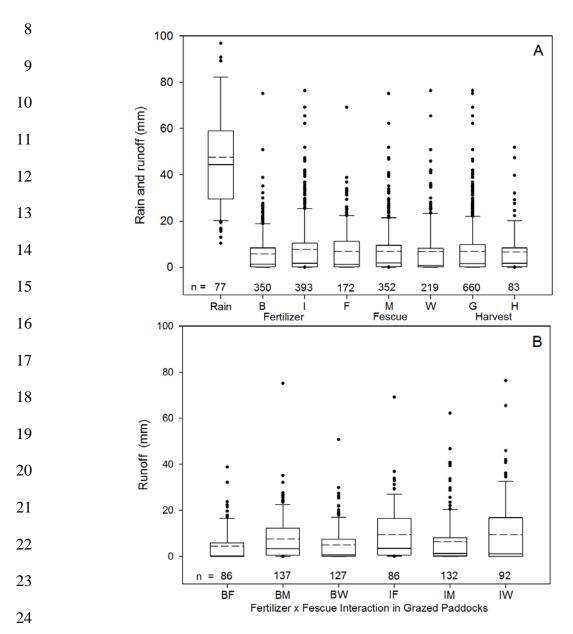


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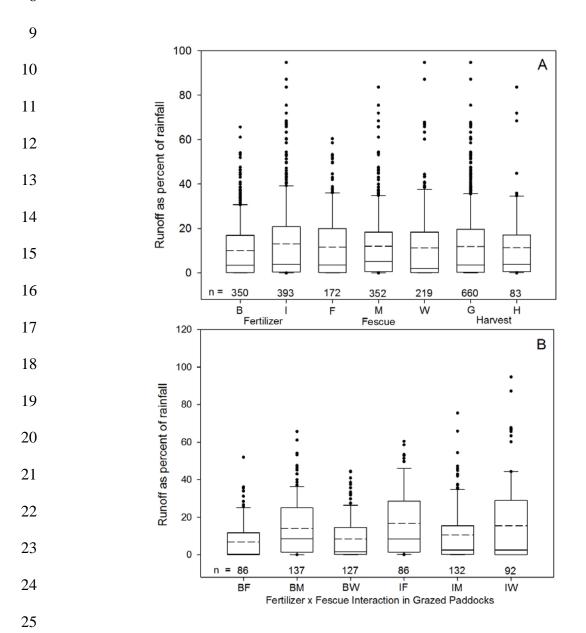


Box plots for runoff by treatment using the untransformed dataset with missing values filled in through regression. The mean and median values are represented by the dashed and solid lines, respectively, inside the boxes that bound the 25<sup>th</sup> and 75<sup>th</sup> percentile values. The dots represent values outside of the 10<sup>th</sup> and 90<sup>th</sup> percentile (represented by whiskers).

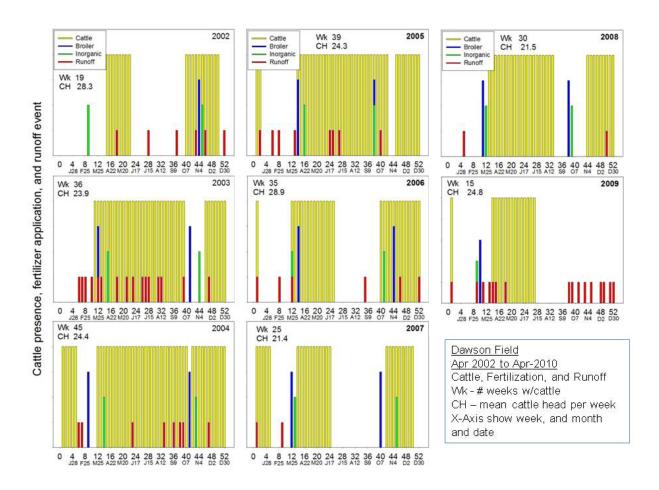




Box plots for runoff as percent of event rainfall by treatment using the untransformed dataset with missing values filled in through regression. The mean and median values are represented by the dashed and solid lines, respectively, inside the boxes that bound the 25<sup>th</sup> and 75<sup>th</sup> percentile values. The dots represent values outside of the 10<sup>th</sup> and 90<sup>th</sup> percentile (represented by whiskers).



Cattle presence, and fertilization and runoff events, April 2002 to April 2010 at Dawson Field paddocks. There were no cattle and no fertilization in 2010; but there were 4 runoff events through April 2010 - (study ended April 2010).



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